

Power and Heat Fluctuation Theorems for Electric Circuits

R. van Zon,¹ S. Ciliberto,² and E. G. D. Cohen¹

¹The Rockefeller University, 1230 York Avenue, New York, New York 10021, USA

²Laboratoire de Physique, CNRS UMR 5672, Ecole Normale Supérieure de Lyon, 46 Allée d'Italie, 69364 Lyon CEDEX 07, France

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Using recent fluctuation theorems from nonequilibrium statistical mechanics, we extend the theory for voltage fluctuations in electric circuits to power and heat fluctuations. They could be of particular relevance for the functioning of small circuits. This is done for a parallel resistor and capacitor with a constant current source for which we use the analogy with a Brownian particle dragged through a fluid by a moving harmonic potential, where circuit-specific analogs are needed on top of the Brownian-Nyquist analogy. The results may also hold for other circuits as another example shows.

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Nanotechnology is quickly getting within reach, but the physics at these scales could be different from that at the macroscopic scale. In particular, large fluctuations will occur, with mostly unknown consequences. In this Letter, we will investigate properties of electric circuits concerning the fluctuations of power and heat within the context of the so-called *fluctuation theorems* (FTs). These theorems were originally found in the context of non-equilibrium dynamical systems theory. Surprisingly, they can also be applied to electric circuits, as we will show, and thus give further insight into their behavior.

Let us first give a brief introduction to the FTs. First found in dynamical systems [1,2] and later extended to stochastic systems [3], these conventional FTs give a relation between the probabilities to observe a positive value of the (time averaged) “entropy production rate” and a negative one. This relation is of the form $P(\sigma)/P(-\sigma) = \exp[\sigma\tau]$, where σ and $-\sigma$ are equal but opposite values for the entropy production rate, $P(\sigma)$ and $P(-\sigma)$ give their probabilities, and τ is the length of the interval over which σ is measured. In these systems, the above-mentioned FT is derived for a mathematical quantity σ , which has a form similar to that of the entropy production rate in irreversible thermodynamics.

Apart from an early experiment in a turbulent flow [4], for quite some time the investigations of the FTs were restricted to theoretical approaches and simulations. In 2002, Wang *et al.* performed an experiment on a micron-sized Brownian particle dragged through water by a moving optical tweezer. In this experiment, a *transient fluctuation theorem* (TFT) was demonstrated for fluctuations of the total external work done on the system in the transient state of the system, i.e., considering a time interval of duration τ which starts immediately after the tweezer has been set in motion [5]. In contrast, a *stationary state fluctuation theorem* (SSFT), which was not measured, would concern fluctuations in the stationary state, i.e., in intervals of duration τ starting at a time long after the tweezer has been set in motion. While the *work* fluctuations satisfy the conventional TFT and SSFT

[6,7], the *heat* fluctuations satisfy different, extended FTs due to the interplay of the stochastic motion of the fluid with the deterministic harmonic potential induced by the optical tweezer [8,9]. Given the possible problems with identifying the entropy production [5,7], in this Letter we prefer to consider the work and the heat.

We remark that the *conventional* FTs hold in time-reversible, chaotic dynamical systems [1,2] and in finite stochastic systems if transitions can occur forward and backward [3]. However, the general condition for an *extended* FT is unknown.

In view of the well-known analogy of Brownian motion (as in the experiment of Wang *et al.*) and Nyquist noise in electric circuits [10], one could ask whether the TFT and SSFT based on the Langevin equation also apply to electric circuits. Electric circuits are interesting as they are directly relevant to nanotechnology and because they lend themselves easily to experiments. Indeed, it turns out the conventional FTs hold for *work* and the extended FTs for *heat*, as we will show here. We emphasize that, to connect with previous papers on which this one is based, we will also use the term *work* for the electric circuits, which is nothing but the time integral of the *power*.

To exploit the analogy of the Langevin descriptions for electric circuits and that of the Brownian particle, we first recall the form of the Langevin equation for the Brownian particle in the experiment of Wang *et al.* [6]:

$$m \frac{d^2 x_t}{dt^2} = -\alpha \frac{dx_t}{dt} + \xi_t - k(x_t - v^* t). \quad (1)$$

Here, m is the mass of the Brownian particle, x_t is its position at time t , α is the (Stokes’) friction coefficient, k is the strength of the harmonic potential induced by the optical tweezer, and v^* is the constant speed at which the tweezer is moved. ξ_t represents a Gaussian white noise, which satisfies

$$\langle \xi_t \rangle = 0, \quad \langle \xi_t \xi_{t'} \rangle = 2k_B T \alpha \delta(t - t'), \quad (2)$$

where $\langle \rangle$ denotes an average over an ensemble of similar

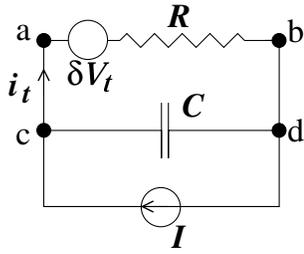


FIG. 1. Circuit with Nyquist noise and a resistor and capacitor in parallel, subject to a current source.

systems [10], T is the temperature of the water, and k_B is Boltzmann's constant. Usually, the velocity relaxes quickly, so one can set $m = 0$ in Eq. (1).

Next we consider in Fig. 1 an electric circuit in which a resistor with resistance R and a capacitor with capacitance C are arranged *in parallel* and are subject to a constant, nonfluctuating current source I . Energy is being dissipated in the resistor, and according to the fluctuation-dissipation theorem this means there are fluctuations also. To a good approximation, one can use a Gaussian random noise term δV_t to describe these fluctuations [10], which is depicted in the figure by a voltage generator. In addition, we define q_t as the charge that has gone through the resistor, i_t as the current that is going through it (so $i_t = dq_t/dt$), and q'_t as the charge on the capacitor, all at time t . Using $q'_t = \int_0^t dt' (I - i_{t'}) = It - q_t$ and $V_{ab} = q'_t/C$, standard calculations for electric circuits give

$$0 = -R \frac{dq_t}{dt} - \delta V_t - \frac{q_t - It}{C}, \quad (3)$$

in which δV_t satisfies [10]

$$\langle \delta V_t \rangle = 0, \quad \langle \delta V_t \delta V_{t'} \rangle = 2k_B T R \delta(t - t'). \quad (4)$$

We see that Eqs. (3) and (4) are of a very similar form as those for a one-dimensional massless Brownian particle dragged through a fluid by means of a harmonic potential in Eqs. (1) and (2) [11]. Table I gives all the analogs, i.e., both the well-known Brownian motion-Nyquist noise ones (ξ_t , α , T vs δV_t , R , T) as well as additional circuit-specific ones.

Given this analogy, we turn to the *heat* fluctuations in this circuit. This heat is developed in the resistor. Thus, the dissipated heat over a time τ is given by the time integral of the voltage over the resistor, V_{ab} , times the current through it, i_t ; i.e.,

$$Q_\tau = \int_0^\tau dt i_t [i_t R + \delta V_t] = - \int_0^\tau dt i_t \frac{q_t - It}{C}, \quad (5)$$

where we used Eq. (3). This is precisely the quantity found in Refs. [8,9] for the Brownian particle, when we use the analogies in Table I. Hence, Q_τ in this parallel RC circuit behaves completely analogous to the heat for the Brownian particle, and thus we know that it satisfies the extended FT. That is, defining a *fluctuation function* by

$$f_\tau^Q \equiv \frac{k_B T}{\langle Q_\tau \rangle} \ln \left[\frac{P(+Q_\tau)}{P(-Q_\tau)} \right] \quad (6)$$

and a scaled heat fluctuation by $p_Q \equiv Q_\tau / \langle Q_\tau \rangle$, one has for large τ

$$f_\tau^Q(p_Q) = \begin{cases} p_Q + O(\tau^{-1}) & \text{if } 0 < p_Q < 1 \\ p_Q - \frac{1}{4}(p_Q - 1)^2 + O(\tau^{-1}) & \text{if } 1 < p_Q < 3 \\ 2 + O(\sqrt{(p_Q - 3)/\tau}) & \text{if } p_Q > 3. \end{cases} \quad (7)$$

Here, we gave only the orders of magnitude of the finite- τ correction terms. Their detailed forms—which differ in the transient and the stationary state—require an involved calculation using the saddle point method which can be found in Ref. [9]. Note that, because of our construction of an analogy between this system and the dragged Brownian particle, this calculation need not be redone for the current case, but that we can make the substitutions in Table I and in footnote 24 of Ref. [9].

Next, we discuss the *work* fluctuations in this circuit. The total work done in the circuit is the time integral of the power. The power is the current through the circuit, I , times the voltage over the whole circuit, V_{cd} , so that

$$W_\tau = \int_0^\tau dt I \left[-\frac{q_t - It}{C} \right]. \quad (8)$$

This happens to be precisely the form of the work as we found in the Brownian case [6], if we use Table I. This is somewhat surprising because those analogs were based on Eq. (3), which in principle involves only the current through the resistor, while W_τ is the work done on the whole circuit. Since the work fluctuations for the Brownian particle satisfy the conventional FT for $\tau \rightarrow \infty$ [6,7], by analogy we know the same will hold here; i.e.,

$$f_\tau^W \equiv \frac{k_B T}{\langle W_\tau \rangle} \ln \left[\frac{P(+W_\tau)}{P(-W_\tau)} \right] = \frac{p_W}{1 - \varepsilon(\tau)}, \quad (9)$$

where $p_W = W_\tau / \langle W_\tau \rangle$. Here, for the TFT, $\varepsilon = 0$ while for the SSFT (for details see Ref. [6])

$$\varepsilon(\tau) = 1 - \frac{\langle [W_\tau - \langle W_\tau \rangle]^2 \rangle}{2\langle W_\tau \rangle} = \frac{\tau_r (1 - e^{-\tau/\tau_r})}{\tau}, \quad (10)$$

where $\tau_r = RC$. Note that $\varepsilon(\tau) \rightarrow 0$ for $\tau \rightarrow \infty$.

We note that the behavior of the heat fluctuations in Eq. (7) differs from that of the work fluctuations in Eq. (9)

TABLE I. The analogy of a circuit and a Brownian particle.

Brownian particle	ξ_t	α	T	x_t	v_t	k	v^*
RC circuits	$-\delta V_t$	R	T	q_t	i_t	$1/C$	Parallel: I Serial: CA

due to exponential tails of the distribution of heat fluctuations [8,9], while those of $P(W_\tau)$ are Gaussian.

A second example of a circuit that satisfies the extended heat fluctuation theorem is depicted in Fig. 2. Here, the resistor with resistance R and the capacitor with capacitance C are arranged *in series* and are subject to a linearly increasing voltage source $V(t) = At$. Again, there is a thermal noise generator next to the resistance. The definitions of i_t and q_t are still that they are the current and charge through R at time t , respectively, but $q'_t = q_t$ here, since all charge that runs through R ends up in C . We find the appropriate Langevin equation as follows. The imposed voltage, $V(t)$, is equal to the potential difference $V_{ad} = i_t R + \delta V_t + q_t/C$ (cf. Fig. 2). Using $i_t = dq_t/dt$ and $V(t) = At$, we find

$$0 = -R \frac{dq_t}{dt} - \delta V_t - \frac{q_t - CA t}{C}. \quad (11)$$

This equation is the same as that of Eq. (3) except that I is replaced by CA . This means that, as far as the current through the resistance is concerned, a constant current source with a capacitor in parallel to it is equivalent to a linearly increasing voltage with a capacitor in series with it. It also means that this case is analogous to the Brownian particle dragged through a fluid by a harmonic potential as well. Quantities for this circuit and the Brownian model can therefore be translated into each other using Table I, except for the work, as we will explain below.

Consider now the *heat* developed in the resistor during a time τ , which is given by the time integral of the voltage over the resistor, V_{ab} , times the current through it, i_t , so

$$Q_\tau = \int_0^\tau dt i_t [i_t R + \delta V] = - \int_0^\tau dt i_t \frac{q_t - CA t}{C}, \quad (12)$$

where we used Eq. (11). Note that, using $I \sim CA$, this form for Q_τ is the same as in Eq. (5) for the parallel case. Hence, the heat in the serial case behaves precisely the same as in the parallel circuit, because we have seen that q_t and i_t behave the same in both circuits. Thus, we know that the heat in the serial RC circuit, in the parallel RC circuit, and in the Brownian system all behave analogously, and all satisfy the extended FT [8,9] in Eq. (7).

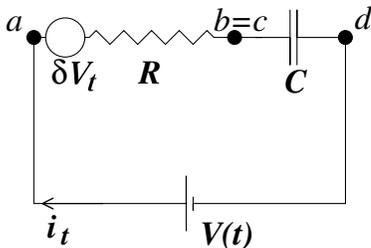


FIG. 2. Serial RC circuit with Nyquist noise and imposed voltage.

We will now consider the *work* fluctuations in the serial RC circuit. The work is the time integral of the total current, i_t , times the total voltage, $V(t) = At$; hence,

$$W_\tau^* = \int_0^\tau dt i_t At. \quad (13)$$

Even when we use $I \sim CA$, this is not of the same form as W_τ in Eq. (8) (which is why we added a superscript *), and likewise, using Table I, it is not of the same form as in the Brownian case. Only in equilibrium are the two RC circuits completely equivalent, since then $I = CA = 0$ and $W_\tau = W_\tau^* = 0$. Clearly, out of equilibrium, we cannot use the same results for W_τ^* as we obtained for W_τ from the Brownian case or the parallel circuit: We in fact need an additional calculation. For this, we use the method in Ref. [6]. For a Gaussian $P(W_\tau^*)$ one has

$$f_\tau^{W^*} \equiv \frac{k_B T}{\langle W_\tau^* \rangle} \ln \left[\frac{P(+W_\tau^*)}{P(-W_\tau^*)} \right] = \frac{p_W^*}{1 - \varepsilon(\tau)}, \quad (14)$$

where $p_W^* = W_\tau^*/\langle W_\tau^* \rangle$ and $\varepsilon(\tau) = 1 - V/(2M)$ with $M = \langle W_\tau^* \rangle$ and $V = \langle (W_\tau^* - \langle W_\tau^* \rangle)^2 \rangle$. The quantities M and V in turn are calculated using the definition of W_τ^* in Eq. (13) and the relations $\langle q_t \rangle = CA[t - \tau_r(1 - e^{-t/\tau_r})]$ and $\langle (q_t - \langle q_t \rangle)(q_{t'} - \langle q_{t'} \rangle) \rangle = k_B T C e^{-|t-t'|/\tau_r}$ (from Ref. [6], using Table I). This yields

$$\varepsilon(\tau) = 2 \frac{\tau_r^2(1 - e^{-\tau/\tau_r}) - \tau \tau_r e^{-\tau/\tau_r}}{\tau^2}. \quad (15)$$

Note that this goes to zero asymptotically as $1/\tau^2$, which is faster than the $1/\tau$ decay of $\varepsilon(\tau)$ in Eq. (10).

These results thus far made no explicit reference to nanoscale circuits. Indeed, these results are valid for a circuit of any size. We will now turn to their relevance for nanocircuits. The extended FT shows that large heat fluctuations are more likely to occur than according to the conventional FT, due to the exponential tails of the distribution of heat fluctuations. This could be important for the design of nanostructures because of the rise of temperature due to heat development. Either the *average* current through R could be too large or a *large heat fluctuation* might occur. Fluctuations of the energy exist already in an equilibrium system in contact with a heat reservoir, i.e., a circuit for which $I = 0$. In that case, the energy fluctuations of an N atomic resistor will be of the order of $\sqrt{N}k_B T$. To explore the properties of nanostructures, composed of just a few atoms, we start with $N = 1$. For that case, energy fluctuations are of the order of $k_B T$ which, if they were not removed, could amount to a significant increase or decrease of the resistor's temperature. An estimate of this temperature change can be made using the law of Dulong and Petit that (at room temperatures) the specific heat per atom of a solid is $3k_B$. Thus, the change in temperature could be as large as $\Delta T = k_B T/(3k_B) = T/3 = 100$ K, for $T = 300$ K.

In our Langevin theory for the circuits, we have assumed a constant temperature. To still be able to use the theory, we need the temperature not to vary too much. A similar condition is needed if the resistor is not to fail. To satisfy this condition, the heat developed will have to be transported away at a fast enough time scale τ_T . If the heat Q_{τ_T} developed in this time is large enough to significantly increase the material's temperature, failure may occur. The induced temperature difference, given by $\Delta T = Q_{\tau_T}/C_V$, is insignificant if $\Delta T/T \ll 1$, i.e., if

$$\frac{Q_{\tau_T}}{C_V T} \ll 1. \quad (16)$$

This condition should hold both for the average and the fluctuations of Q_{τ_T} . Let us first consider the average (i.e., what one would do for macroscopic circuits). In the stationary state of the parallel circuit, the average heat is $Q_{\tau_T} = IV\tau_T$, where $V = IR$, so

$$\frac{Q_{\tau_T}}{C_V T} = \frac{I^2 R \tau_T}{C_V T} = \frac{\tau_T}{\tau_H}, \quad (17)$$

where $\tau_H = C_V T/I^2 R$. (This in fact also holds for the serial circuit if we replace I by CA .) Equation (16) now becomes

$$\tau_T \ll \tau_H. \quad (18)$$

That is, the time scale of temperature relaxation given by τ_T has to be fast compared to the heating time τ_H . However, even if the average of the heat is well behaved, the heat fluctuations might still damage the circuit. We need the typical size of these fluctuations. From our previous work on the FTs, we found that, for long times τ , $\sqrt{\langle(Q_\tau - \langle Q_\tau \rangle)^2\rangle} \approx \sqrt{2k_B T \langle Q_\tau \rangle}$ [8,9]. Thus, for $\tau = \tau_T$, $\sqrt{2k_B T I^2 R \tau_T}$ is a typical value for Q_{τ_T} which we can insert into Eq. (16), giving

$$\frac{2k_B I^2 R \tau_T}{T C_V^2} \equiv \frac{\tau_T}{\tau_F} \ll 1, \quad (19)$$

where the time scale for the heat fluctuations is $\tau_F = T C_V^2 / 2k_B I^2 R = (C_V / 2k_B) \tau_H$. For an N atomic solid at room temperature, for which Dulong-Petit is valid, we know that $\tau_F / \tau_H = C_V / 2k_B = \frac{3}{2} N$. Thus, the factor between τ_F and τ_H is always bigger than one, so that Eq. (19) in fact follows from Eq. (18). As a result, if on average the circuit will not fail, then the fluctuations will not make it fail either. However, for systems below room temperature, for which quantum effects become relevant, the ratio C_V / k_B can be much smaller than 1 (i.e., Debye's law), opening up the possibility that in that case the requirement on τ_F in Eq. (19) could be stricter than that on τ_H in Eq. (18).

Although reassuring, Eq. (19) concerns only typical fluctuations. However, one also needs to be concerned

with large fluctuations. Compared to the Gaussian distributed work (or power) fluctuations, large fluctuations for heat are much more likely due to the exponential tails of its distribution function. Furthermore, if the condition in Eq. (16) is not met, temperature variations will occur and the theory then needs to include a coupling to the heat diffusion equation. This could be relevant for future experiments.

In conclusion, we studied work and heat fluctuations in electric circuits using analogies to Brownian systems with nonuniversal additions to the Nyquist noise-Brownian motion analogy. Our analogy links the work and heat fluctuations in a parallel RC circuit to those in a Brownian system for which the work and heat fluctuations are known to satisfy the conventional FT and extended FT, respectively. For the serial circuit, the analogy also works for the heat fluctuations, but not for the work fluctuations. However, a short calculation [below Eq. (13)] shows they still satisfy the conventional FT.

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